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# Hydrodynamic Voltammetry of Fe<sup>2+/3+</sup> in Aqueous Deep Eutectic Solvents Towards Redox Flow Batteries

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## **Abstract**

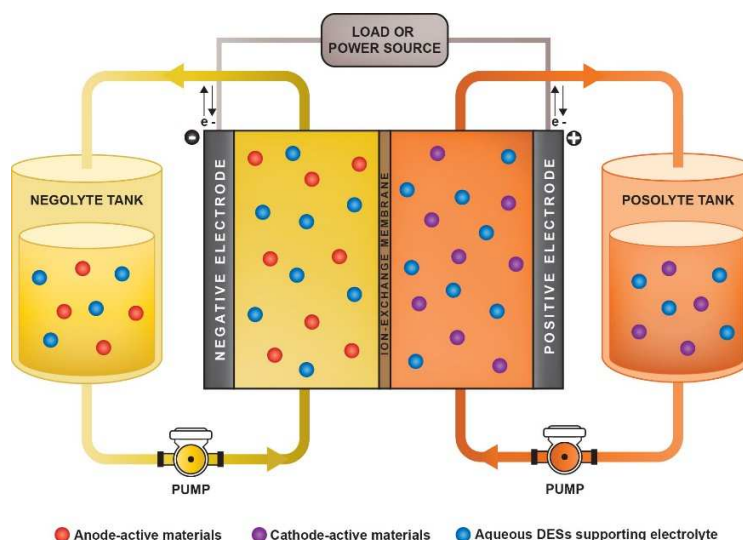
Deep eutectic solvents (DESs) have recently attracted much attention as potential green electrolyte solvents for redox flow batteries. DESs are considered not only as environmentally sustainable but also economically attractive electrolytes because they can be resourced from biological feedstock (alcohols, urea, choline) and are earth-abundant and of low toxicity. Despite these advantages, DESs still have limitations in important aspects such as reactant and ion transport, which is inhibited due to hydrogen-bonding-induced viscosity. Thus, improving the transport properties of redox species in DESs is essential. In addition, we explore the quantitative addition of water to ethaline (a 1:2 choline chloride: ethylene glycol mixture) in order to understand its influence on the kinetics and mass transport properties of DESs. In this work, we show that DESs can be made more fluid and less dense, while avoiding most of the electrochemical instabilities of water. Herein, we investigate the effects of gradually increasing amounts of water to the redox system of  $\text{Fe}^{2+/3+}$  in ethaline. Our study shows that systematic addition of water leads to a three-fold increase in ionic conductivity and decrease in viscosity that enhances the mass transport and kinetics of DES-based electrolytes while still maintaining an electrochemical window of approximately 1.90 V. The use of environmentally benign electrolyte components together with the observed increase in conductivity will result in a more efficient redox flow battery (RFB) that operates at higher power density without relying on harmful solvents and fossil fuel-based processes.

**Keywords:** deep eutectic solvent; redox flow battery; hydrodynamic voltammetry; redox couple; renewable energy

## 1. Introduction

The increasing global energy demand and related carbon dioxide emissions have spurred interest in the transition from traditional fossil fuels to renewable energies, which are most common in the form of solar and wind energies.[1,2] Although solar and wind energies have the advantage of being low-carbon and long-term energy sources; they suffer from being inherently intermittent and less flexible.[3,4] To address these challenges, various energy storage systems can be integrated with a renewable energy source.[5] For example, pump hydroelectric storage dominates the existing energy storage systems. However, it is limited by the very large land footprint as it requires to build two large reservoirs at different elevations. Considering other energy storage systems, redox flow batteries (RFBs) store more energy while delivering high power loads compared to conventional batteries. [6] In comparison with the lithium-ion battery that has attracted commercial attention, RFBs are potentially of lower cost, longer lifetime, safer, and easier to recycle.[5,7]

In a typical RFB, the electrolyte containing the active species is stored in two external tanks as seen in Scheme 1. One tank is for the storage of the negative electrolyte, and the other tank is for the storage of the positive electrolyte.[8] During operation, the electrolytes are pumped into the flow battery stack, which has positive and negative electrode compartments. These two fluids are separated by an ion-exchange membrane which allows the charge carriers to move between two electrolytes to balance the charge during operation while restricting the mixing of the two electrolytes. Energy can then either be stored or extracted from the RFB by changing the oxidation state of electrolyte fluids.[9] Hence, the electrolyte is an essential part of the RFB. It closes the electronic and ionic circuit between the anode and cathode. In a liquid flowing electrolyte systems like in an RFB, low-viscosity electrolyte is essential to yield a faster ionic transport and enhanced ionic conductivity.



**Scheme 1.** Schematic diagram of a redox flow battery. The active materials and the supporting electrolytes are stored in the external electrolyte tanks. In RFBs, increased electrolyte fluidity is desired to improve the ion mobility and conductivity of electroactive species.

Deep eutectic solvents (DESs) gained attention as potential suitable green electrolytes for RFBs.[10–12] DESs are an emerging class of mixtures of hydrogen-bond donor molecules and hydrogen-bond acceptor molecules that are characterized by a significant depression of its melting point compared to that of its individual constituents.[13] They share properties with ionic liquids (ILs), such as low volatility, high thermal and chemical stability, and tunable polarity.[14,15] However, DESs possess additional advantages, which includes low cost, non-toxicity, and ease of preparation.[16,17] On the other hand, DESs being non-aqueous electrolytes, often have limited solubility for electroactive species due to the low solvent dielectric constant. This can be improved by using electroactive salts such as iron chlorides as the hydrogen-bond acceptor,[18] or even functionalizing the constituent molecules of the DES with electroactive groups.[19–21] The dynamics and electrokinetics of various electroactive salts in traditional liquid electrolytes, such as aqueous and organic electrolytes, have already been established.[22–25] However, these electrolytes are limited by their narrow potential window, high volatility, and high toxicity, which

makes them not ideal for RFB applications.[26,27] Investigating the use of completely replenishable and sustainable electrolyte components is necessary for future energy storage and conversion.

DESs can be made by sustainable processes, [28] but suffer from physical limitations of high viscosity, and consequently, low ionic conductivity, and diffusivity of redox active species.[29] To address these constraints, incorporation of minor amounts of water can be exploited since it disrupts the strong hydrogen bond network between the DES components,[30] which can reduce the viscosity and enhance transport properties. This work aims to study the analytical addition of water as a minority solvent component to the DESs and its effects on transport kinetics. We examine the effect of water addition on DES by electrochemical measurements including electrochemical impedance spectroscopy, cyclic voltammetry, and linear sweep voltammetry of the well-established redox couple  $\text{Fe}^{2+/3+}$  for reference. A systematic addition of water lowers viscosity, increases ionic conductivity and diffusion coefficients, reduces density, while preserving the electrochemical stability window. This study reveals that the addition of analytical amounts of water to eutectic solvent mixtures provides a technologically viable basis for improving flow battery performance.

## **2. Experimental methods**

### *2.1. Chemical reagents*

The anhydrous ethylene glycol (EG,  $\geq 99\%$  purity), choline chloride (ChCl,  $\geq 99\%$  purity), and anhydrous iron (II) chloride ( $\text{FeCl}_2$ , 98% purity) were purchased from Sigma Aldrich. The anhydrous iron (III) chloride ( $\text{FeCl}_3$ , 98% purity) was purchased from Fischer Scientific. The

water used in this experiment was purified using a Millipore Milli-Q system to a resistivity of 18.2 M $\Omega$  cm.

## *2.2. Sample preparation*

The ethylene glycol was dried using activated molecular sieve for 48 h while the choline chloride was dried under vacuum for 48h at 373 K to remove adsorbed water. The dried choline chloride and ethylene glycol were mixed in a 1:2 molar ratio inside an argon-filled glovebox to produce a DES which is commonly named ethaline. The DES mixture was then placed in a sonicator for 30 min at 303 K to generate a clear ethaline solution which subsequently was cooled to room temperature. After that, FeCl<sub>2</sub> and FeCl<sub>3</sub> were dissolved in the previously prepared ethaline to a concentration of 50 mM FeCl<sub>2</sub> and 50 mM FeCl<sub>3</sub>. To completely dissolve the iron salts, the mixture was heated to 303 K. Then predetermined amounts of water were added to the mixture to make 5, 10, and 25 wt.% added water samples. The FeCl<sub>2</sub> and FeCl<sub>3</sub> in aqueous-containing ethaline solution was then transferred and sealed into a 5-necked double-walled electrochemical cell. To minimize water adsorption from the atmosphere, the solution was saturated with high-purity nitrogen (N<sub>2</sub>) gas throughout the measurements.

## *2.3. Water content determination*

Karl Fischer titration (Metrohm Coulometer 899) was performed to provide a baseline for the water content in ethaline as base solvent without any additional water. That baseline water content was found to be below 1500 ppm.

## *2.4. Viscosity and density measurements.*

A Rheosense microviscometer was used to measure the viscosity of the samples using a microfluidic chip calibrated for the range 1-100 cP. To measure the temperature-dependent viscosity of the samples, a Rheosense temperature controller was utilized. Density

measurements were taken using an Anton Paar density meter (DMA 5000 M) at temperatures in the range of 298– 323 K in 5 K increments.

### 2.5. Conductivity measurements

Electrochemical impedance spectroscopy (EIS) was utilized to determine the conductivity of the samples. A cell with two platinum electrodes was filled with sample solutions. The impedance measurements were performed at 100 – 10,000 Hz to obtain a Nyquist plot. The solution resistances ( $R_s$ ) of the samples were then determined by estimating where the high frequency data intercepts the real resistance axis. Using the measured resistance, the conductivity of samples was calculated using the eq. (1).

$$\sigma (mS \cdot cm^{-1}) = \frac{k (cm^{-1})}{\rho (ohm)} \times 1000 \quad (1)$$

where  $\sigma$  is the conductivity,  $k$  the cell constant, and  $\rho$  is the solution resistance. The cell constant of the platinized cell was  $1.0 \text{ cm}^{-1}$ . To measure the conductivity of the samples at a controlled temperature, the cell was submerged in mineral oil heated on a digital hot plate with temperature probe.

The molar conductivity of the samples was calculated by plugging the measured conductivity values to eq. (2).

$$\Lambda (S \cdot cm^2 \cdot mol^{-1}) = \frac{\sigma (S \cdot cm^{-1})}{c (mol \cdot cm^{-3})} \quad (2)$$

where  $\Lambda$  is the molar conductivity,  $\sigma$  is the measured conductivity, and  $c$  is the molar concentration of the samples.

The viscosity, density, and conductivity data of the samples in the temperature range from 298 K to 323 K in 5 K increments are reported in Table S1.

### 2.6. Cyclic voltammetry (CV) and linear sweep voltammetry (LSV)



Cyclic voltammetry was performed at  $100 \text{ mV s}^{-1}$ , sweeping to positive potentials first from 0 V vs. the reference electrode. Electrolyte samples of 100 mL were placed in a multiport glass electrochemical cell with a 5 mm platinum (Pt) disc as the working electrode, a graphite rod as the counter electrode, and Pt/Fe<sup>2+</sup>/Fe<sup>3+</sup> (Pt RE) as the reference electrode. The Pt RE is constructed by introducing a platinized Pt wire into a Luggin capillary filled with a 50 mM FeCl<sub>2</sub>/FeCl<sub>3</sub> ethaline electrolyte. The Luggin capillary is designed to have an opening near the working electrode, which allows the test solution to come in contact with the electrolyte. Electrochemical tests were controlled with a Biologic SP-240 potentiostat.

Utilizing the data obtained from the CV curves, the electrochemical stability window is determined employing eq. (3).

$$E_{\text{sw}} = E_{\text{an}} - E_{\text{cat}} \quad (3)$$

where  $E_{\text{sw}}$  is the electrochemical stability window,  $E_{\text{an}}$  is the anodic oxidation potential limit, and  $E_{\text{cat}}$  is the cathodic reduction potential limit.

For the linear sweep voltammetry, the same set-up was used with the sweeping rate set at  $10 \text{ mV s}^{-1}$ . The rotating disk electrode was spun at 900, 1200, 1600, 2000, 2200, and 2500 rpm using a Pine Instruments MSR rotator. All the electrochemical experiments were conducted in the temperature range of 298 – 323 K in 5 K increments using circulating water bath to stabilize each temperature.

## 2.7. Nuclear magnetic resonance (NMR) spectroscopy

The samples for NMR measurements were prepared by dissolving dry or water-containing Fe<sup>2+/3+</sup>-ethaline solutions in deuterium oxide (D<sub>2</sub>O) at a ratio of 1:1 after they were exposed to a potential bias of 350 mV beyond anodic and cathodic limiting voltage at which decomposition occurred in ethaline-water mixtures. A 500 MHz Bruker-Bio Spin Avance III HD spectrometer

fitted with an incredibly high sensitivity Multinuclear Broadband CryoProbe was used to obtain NMR spectra at 298 K. The measurements of  $^1\text{H}$ -NMR, and  $^{13}\text{C}$ -NMR were taken using the operational magnetic field of 11.7 T.

### 2.8. Atomic absorption spectroscopy (AAS)

The solubility of  $\text{FeCl}_2/\text{FeCl}_3$  in the samples was measured by saturating the samples with the iron chloride salts until no more salt dissolved after sonication at 298 K for 2 hours. An Agilent 240 FS flame atomic absorption spectrometer was then utilized to measure the concentration of Fe ions dissolved in the saturated samples. An Fe hollow cathode lamp operating at 372.0 nm was used as the radiation source. A standard Fe calibration curve was constructed to determine the levels of Fe in the water-containing ethaline samples. This was achieved by utilizing the Agilent's Sample Introduction Pump Systems (SIPS) by performing in-line dilution of 1000 ppm in 2%  $\text{HNO}_3$  stock solution (TraceCERT<sup>®</sup>, Sigma Aldrich), and subjecting the 0, 5, 10, 15, and 25 ppm Fe standard solutions to AAS analysis using a premixed burner air-acetylene flame. The same experimental conditions were then used to analyze the Fe content of the ethaline-water mixtures, with the constructed calibration curve used to determine the concentrations of Fe in each sample.

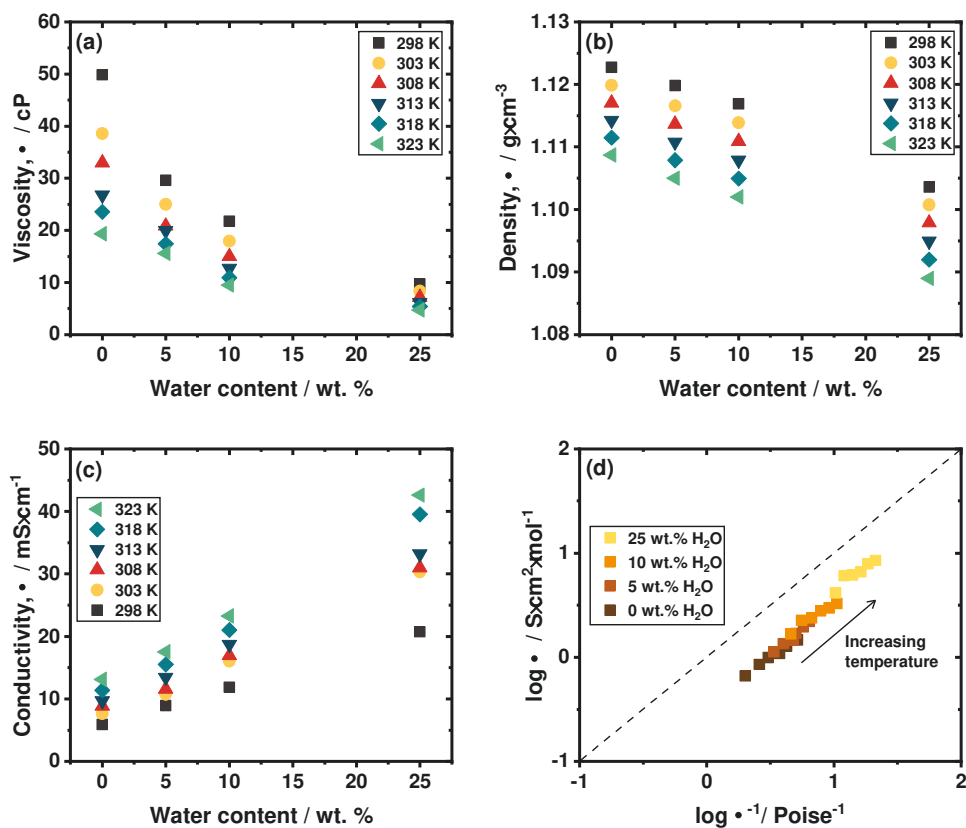
## 3. Results and Discussion

### 3.1. Viscosity, density, ionic conductivity, and Walden plot

To determine the influence of water addition to the transport and kinetics properties of  $\text{Fe}^{2+}$  and  $\text{Fe}^{3+}$  ions in ethaline (a 1:2 mixture of choline chloride and ethylene glycol), 50 mM  $\text{FeCl}_2/\text{FeCl}_3$  was added to all solutions.

In Figure 1a, with gradually increasing amounts of water, the temperature-dependent viscosity of Fe<sup>2+/3+</sup>-ethaline samples decreases. The viscosity of dry Fe<sup>2+/3+</sup>-ethaline at 298 K is 49.85 cP, which is comparable to the previously reported value. [31] Upon addition of 25 wt. % water, the temperature-dependent viscosity of Fe<sup>2+/3+</sup>-ethaline decreased by about 80%. Such a drastic decrease in viscosity can be attributed to the weakening of intermolecular hydrogen bond interactions between the DESs components due to the interference of water.[30] As seen in Figure 1b, as water is added to Fe<sup>2+/3+</sup>-ethaline, the temperature-dependent density of the mixture decreased linearly in the investigated range. Similarly, the fluidity and the ion mobility are expected to increase with water addition, by which the temperature-dependent conductivity is improved as shown in Figure 1c. More than three-fold increase in the temperature-dependent conductivity of Fe<sup>2+/3+</sup> - ethaline is observed upon addition of 25 wt. % water.

In Figure 1d, the Walden plot of temperature-dependent molar conductivity versus fluidity, which is the inverse of viscosity, was plotted to assess the ionicity of the deep eutectic solvent systems. It should be noted that the Walden plot does not specifically take into account the variation in ion sizes. The ideal 0.01 mol L<sup>-1</sup> aqueous KCl line is represented by the dashed line across the origin, which is provided for reference. This reference line represents the case where the ions are completely dissociated and equally mobile.[32] The addition of increasing amounts of water causes a smaller deviation from the reference line, which means that the ionicity of DES increases as more water is added to the mixture. This increase in ionicity supports the significant enhancement in conductivity seen in Figure 1c.



**Figure 1.** Effect of water addition and temperature increase on the (a) viscosity ( $\eta$ ), (b) density ( $\rho$ ), and (c) ionic conductivity ( $\sigma$ ) of Fe<sup>2+/3+</sup>-ethaline solutions. The (d) Walden plot of temperature-dependent molar conductivities ( $\Lambda$ ) and fluidity (inverse of viscosity,  $\eta^{-1}$ ) for water-containing Fe<sup>2+/3+</sup>-ethaline. The dashed line through the origin with a slope of 1 represents the ideal line for 0.01 mol·L<sup>-1</sup> aqueous KCl.

Consequently, an increase in the temperature induces a decrease in viscosity and density, and an increase in conductivity and ionicity as observed in Figure 1a-d. The decrease in viscosity and enhancement in conductivity with increasing temperature has been also observed in previous study.[33] When the temperature was increased from 298 K to 323 K, the conductivity of ethaline increased from 5.91 mS·cm<sup>-1</sup> to 13.15 mS·cm<sup>-1</sup>.

To determine the amount of water that would result in an equivalent increase in conductivity as the temperature range of 298 to 323 K, a linear fit was constructed using the data obtained from the relationship between conductivity and water content, as shown in Figure S1. By employing the

linear fit equation, the water content at which the conductivity reached  $13.15 \text{ mS}\cdot\text{cm}^{-1}$  was determined. This conductivity value is comparable to that obtained by raising the temperature from 298 K to 323 K. The calculated result indicated that achieving a conductivity of  $13.15 \text{ mS}\cdot\text{cm}^{-1}$  would require a water content of 12.15 wt. %. Previous studies have extensively reported on the properties of ethaline-water mixtures in the absence of iron chloride salts, specifically focusing on their viscosity, density, and conductivity. [30,34] Our study investigates the effect of introducing dissolved iron chloride salts into similar compositions of wet ethaline. To assess the impact of these salts on the viscosity, density, and conductivity, a comparative analysis was conducted between the ethaline-water mixture with and without the addition of iron chloride salts, as depicted in Figure S2.

The analysis reveals noteworthy findings: Firstly, the viscosity of the ethaline-water mixture remains unchanged upon the addition of iron chloride salts. Secondly, the density of the mixture shows an increase with the inclusion of iron chloride salts. Lastly, the conductivity of the mixture exhibits a decrease when the salts are introduced, with this trend persisting across the temperature range of 298 to 323 K.

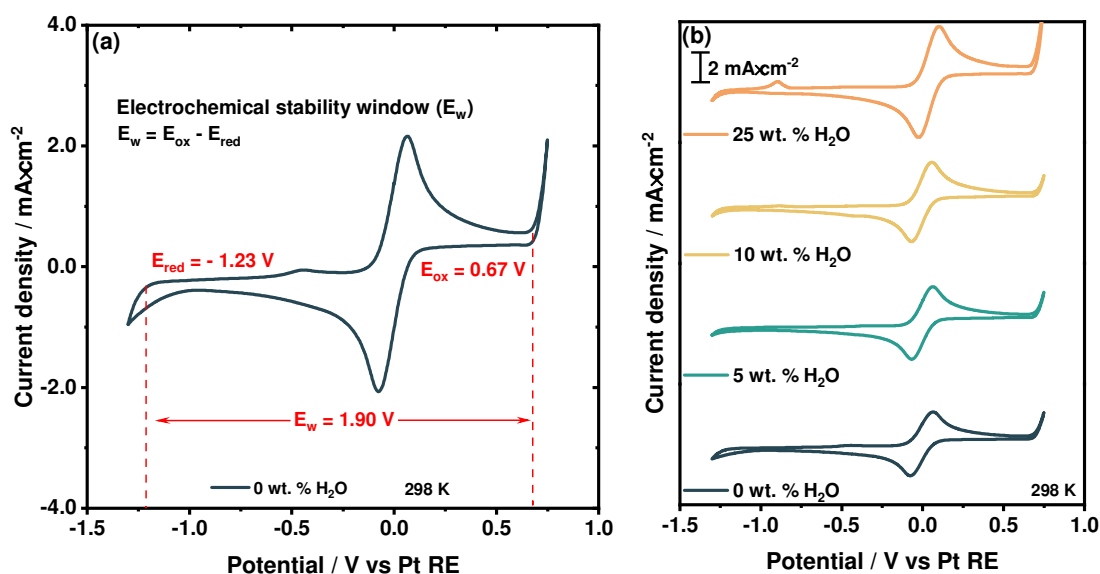
Furthermore, when water is introduced into the mixture, similar trends in viscosity, density, and conductivity are observed, except for the viscosity at a water content of 10 wt. %, where a slight decrease occurs upon the addition of iron chloride salts.

### *3.2. Electrochemical stability window and NMR spectroscopy*

Electrochemical stability window is defined as the voltage range at which the  $\text{Fe}^{2+/3+}$ -ethaline mixtures, containing 0, 5, 10, or 25 wt.% water, show no detectable signs of chemical

decomposition. This electrochemical stability range can be determined using cyclic voltammetry (CV).

The electrochemical stability window ( $E_w$ ) can be extracted from the CV curves using eq. (3), which calculates it as the difference between the anodic oxidation potential limit,  $E_{an}$ , and cathodic reduction potential limit,  $E_{cat}$ . The  $E_{an}$  and the  $E_{cat}$  of  $Fe^{2+/3+}$ -ethaline with 0, 5, 10, or 25 wt. % water at 298 K were determined using the inflection point as illustrated in Figure 2a and as listed in Table 1 together with the calculated  $E_w$ . In Figure 2b, the peaks at potentials  $\pm 0.07$  V vs Pt RE in the CV curves represents the cathodic and anodic currents due to the  $Fe^{2+/3+}$  redox couple. The  $E_w$  of dry  $Fe^{2+/3+}$ -ethaline is 1.90 V, which is lower than the previously reported value.[35] This discrepancy can be attributed to the difference in the working electrodes used in the experiments. Mu and co-workers employed a glassy carbon working electrode, which tends to yield wider  $E_w$  values compared to the platinum working electrode utilized in the current study.[35] The addition of 5 wt. % water in  $Fe^{2+}/Fe^{3+}$ -ethaline decreases the electrochemical window by 20 mV. However, addition of 25 wt. % water decreased the electrochemical window by only 30 mV. The small anodic current related to the oxidation of water appears at around -0.9 V vs Pt RE and is likely related to hydrogen oxidation on the reverse scan following water reduction. The cause for the observed decrease in the electrochemical window of  $Fe^{2+/3+}$ -ethaline upon addition of water is most likely due to the decomposition of  $H_2O$  into  $H_2$  and possibly  $O_2$  gas.[36] In dry ethaline, the cathodic decomposition reaction involves electrochemical hydrolysis of ethylene glycol that produces both hydrogen gas and hydroxyl ions.[37,38] As increasing amounts of water are added to  $Fe^{2+/3+}$ -ethaline, more water tends to decompose to hydrogen and oxygen gases, further narrowing the  $E_w$ .



**Figure 2.** The (a) electrochemical stability windows of the samples were determined by estimating the reduction and oxidation potential limits using the inflection points. (b) CV curves of  $\text{Fe}^{2+/3+}$ -ethaline mixtures containing 0, 5, 10, or 25 wt.%  $\text{H}_2\text{O}$  at a Pt working electrode and at 298 K.

Table 1 shows that the  $E_w$  of the  $\text{Fe}^{2+/3+}$ -ethaline mixture is almost maintained even after addition of 25 wt. % water. This suggests that the ethaline/water mixture studied prevents the water molecules to reach the reactive electrode surface, which seems to be dominated by the organic components with the larger electrochemical window. This preferential electrode surface protection prevents the hydrated DES mixture from decomposition and formation of hydrogen and oxygen gases.

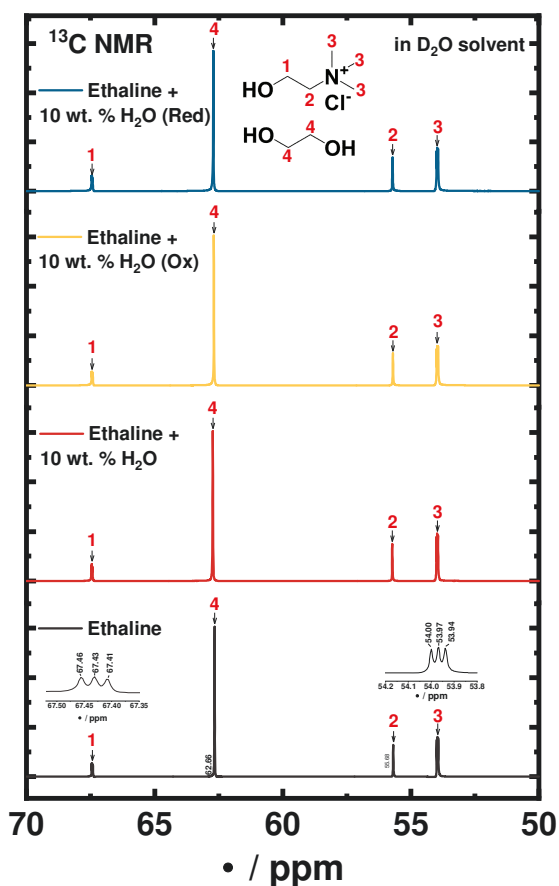
**Table 1.** Cathodic reduction potential limits  $E_{\text{red}}$ , anodic oxidation potential limits  $E_{\text{ox}}$  and electrochemical stability windows  $E_w$  of  $\text{Fe}^{2+/3+}$ -ethaline mixtures containing 0, 5, 10 or 25 wt. %  $\text{H}_2\text{O}$  at 298 K.

Water content (wt. %)	$E_{\text{red}}$ (V vs Pt RE)	$E_{\text{ox}}$ (V vs Pt RE)	$E_w$ (V)
0	-1.23	0.67	1.90
5	-1.23	0.65	1.88
10	-1.22	0.65	1.87
25	-1.22	0.65	1.87

The  $^1\text{H}$  NMR and  $^{13}\text{C}$  NMR analysis studies in  $\text{D}_2\text{O}$  solvent were carried out for an hour after attempted decomposition at biases of 350 mV beyond anodic and cathodic limiting voltage and found no evidence of degradation of the organic ethaline constituents as observed in Figure S3 and Figure 3, respectively. These findings are different from previous results on DES electrochemical degradation.[37] The absence of detectable cathodic or anodic decomposition products in our NMR analysis is due to the relatively mild potential biases (350 mV). While previous studies used harsher conditions to force decomposition, in this study, we were rather interested in making the system work with minimal to no decomposition. The electrochemical degradation products of the HBD and organic salt would only become detectable under harsher electrolysis conditions. Regardless, it is recommended to pursue further research on the electrochemical stability of DES-water mixtures using a wider range of electrochemical conditions. The  $^1\text{H}$  NMR and  $^{13}\text{C}$  NMR relative peak assignments and the corresponding %  $\text{H}_2\text{O}$  in  $\text{D}_2\text{O}$  at 298 K were summarized in Table S2.

The influence of temperature on the  $E_w$  of hydrated  $\text{Fe}^{2+/3+}$ -ethaline mixture was also investigated. As reported in Table S3 and seen in Figure S4, the  $E_w$  of the  $\text{Fe}^{2+/3+}$ -ethaline mixture with the same water quantity became marginally narrower as the temperature increased from 298 K to 323 K, which is expected since the redox reaction is thermally activated. The same trend was observed in the case of DES reline (1:2  $\text{ChCl}$ :urea) with the addition of 1.0 M  $\text{Fe}^{2+/3+}$ , where the  $E_w$  of the mixture became slightly narrower with increasing temperature from room temperature to 323 K. [10]



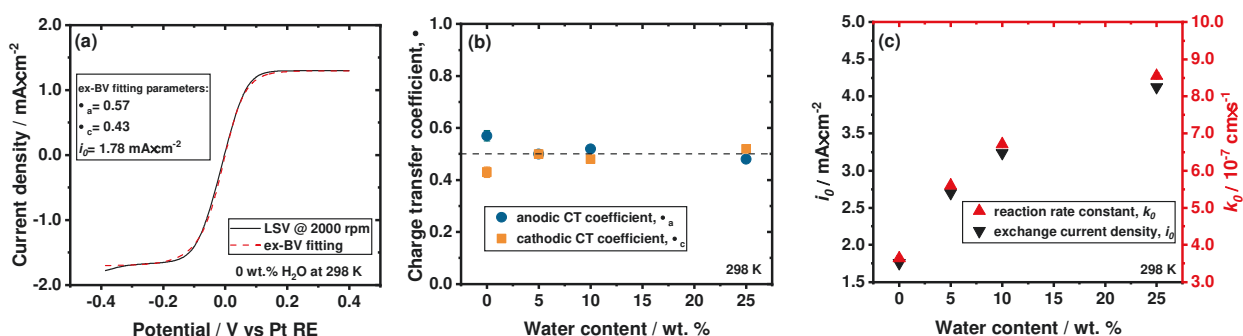


**Figure 3.** <sup>13</sup>C NMR spectra of ethaline, ethaline with 10 wt. % H<sub>2</sub>O, oxidized and reduced ethaline with 10 wt. % H<sub>2</sub>O in D<sub>2</sub>O solvent at 298 K.

### 3.3. Electron transfer kinetics and mass transport properties

The rotating disk electrode (RDE) is used to measure the kinetic properties of the ethaline solutions containing the Fe<sup>2+/3+</sup> redox couple at temperature range of 298 K to 323 K. The RDE consists of a disk-shaped electrode that rotates at a controlled speed in the various Fe<sup>2+/3+</sup>-ethaline solutions.[39] By varying the rotation speed of the disk electrode, the kinetics of Fe<sup>2+/3+</sup> redox reaction can be investigated over a wide range of mass transport conditions. Figure S5-S8 represent the slow-scan linear sweep voltammetry (LSV) measurements of water-containing Fe<sup>2+/3+</sup>-ethaline solutions using Pt RDE at 900 - 2500 rpm rotation speeds. As the rotation speed is increased, the mass transport of the Fe<sup>2+/3+</sup> redox couple to the electrode surface increases, leading to higher

oxidative and reductive current densities. To estimate the charge transfer coefficients and exchange current density from polarization data, the Tafel equation is conventionally used. However, for fast redox reactions in a highly viscous system, a Tafel analysis would not be able to provide accurate estimates of reaction rate parameters. [40]-[41] Thus, here we applied the extended Butler-Volmer (ex-BV) equation to fit the data (Figure S9-S12) to obtain the kinetic parameters as previously proposed by Shen et al.[41] The LSV measured curve and ex-BV fitting of the driest  $\text{Fe}^{2+}/\text{Fe}^{3+}$ -ethaline mixture at rotation speed of 2200 rpm and temperature of 298 K is shown in Figure 4a. The charge transfer coefficients and exchange current density obtained using this ex-BV method at 298 K to 323 K are listed in Table S4.



**Figure 4.** (a) Linear sweep voltammetry curve (solid line) and extended Butler-Volmer fitting (dashed line) of dry  $\text{Fe}^{2+}/\text{Fe}^{3+}$ -ethaline mixture at rotation speed of 2200 rpm at 298 K. The values in the left inset are the anodic charge transfer coefficient ( $\alpha_a$ ), cathodic charge transfer coefficient ( $\alpha_c$ ), and exchange current density of the dry sample as determined using the extended Butler-Volmer fitting. (b)  $\alpha_a$ ,  $\alpha_c$ , (c) exchange current density ( $i_0$ ), and reaction rate constants ( $k_0$ ) of  $\text{Fe}^{2+/3+}$ -ethaline mixture containing 0, 5, 10, or 25 wt. %  $\text{H}_2\text{O}$  at 298 K.

In  $\text{Fe}^{2+}/\text{Fe}^{3+}$ -ethaline solutions, the anodic ( $\alpha_a$ ) and cathodic ( $\alpha_c$ ) charge transfer coefficients describe the efficiency of electron transfer during oxidation ( $\text{Fe}^{2+} \rightarrow \text{Fe}^{3+} + e^-$ ) and reduction ( $\text{Fe}^{3+} + e^- \rightarrow \text{Fe}^{2+}$ ) reactions, respectively. Generally, the values of  $\alpha_a$  and  $\alpha_c$  are between 0 and 1, and a higher value indicates a more efficient electron transfer. It is typically observed that the  $\alpha_a$  is larger than  $\alpha_c$  in the  $\text{Fe}^{2+}/\text{Fe}^{3+}$  because the anodic oxidation reaction is thermodynamically

favorable and occurs more easily than the cathodic reduction reaction, so the efficiency of electron transfer during the anodic oxidation reaction is usually higher than the cathodic reduction reaction.[42] However, the values of  $\alpha_a$  and  $\alpha_c$  can depend on various factors such as the electrode material, the electrolyte composition, and the reaction kinetics, so in some specific cases, it is possible for the  $\alpha_c$  to be larger than the  $\alpha_a$ . In Figure 4b, the  $\alpha_a$  is larger than or equal to  $\alpha_c$  at water content less than or equal to 10 wt. %, which indicates that the electron transfer during oxidation reaction is more efficient than during the reduction reaction at lower water content. With the addition of 25 wt. % water, the  $\alpha_c$  becomes smaller than  $\alpha_a$ , which suggests that electron transfer efficiency is reduced during the oxidation reaction compared to the reduction reaction at higher water content. As shown in Figure S13, the charge transfer coefficients are not noticeably impacted by the increase in temperature, as expected for a simple electron transfer reaction.

The exchange current density ( $i_0$ ) is described as the rate at which  $\text{Fe}^{2+}$  ions are oxidized to  $\text{Fe}^{3+}$  ions and  $\text{Fe}^{3+}$  ions are reduced to  $\text{Fe}^{2+}$  ions at the same electrode surface. In Figure 4c, the  $i_0$  increases nonlinearly with increasing water, which indicates that addition of water facilitates faster electron transfer between the DES electrolyte and the electrodes. Figure S14 shows the significant impact of the temperature on the  $i_0$  of various  $\text{Fe}^{2+}/\text{Fe}^{3+}$ -ethaline solutions due to the temperature dependence of reaction rate constant, which is related to the activation barrier required for the reaction to occur. Increasing the temperature provides more thermal energy to the system which results in more reactant molecules acquiring enough energy to overcome the activation energy barrier needed for the reaction to occur, leading to an increase in the exchange current density.

The reaction rate constant ( $k_{\text{app}}$ ) for the Fe<sup>2+</sup>/Fe<sup>3+</sup>-ethaline solutions represents the rate at which the forward or reverse reaction between Fe<sup>2+</sup> and Fe<sup>3+</sup> ions occurs. Utilizing the  $k_{\text{app}}$  obtained with the extended Butler-Volmer equation,[42] the  $k_{\text{app}}$  can be determined using eq. (4).

$$k_{\text{app}} = \frac{k_{\text{f}}}{1 + \frac{k_{\text{f}}}{k_{\text{b}} \frac{[\text{Fe}^{2+}]}{[\text{Fe}^{3+}]}}} \quad (4)$$

where n is the number of electrons transferred,  $F$  is the Faraday constant (96,485 A s mol<sup>-1</sup>), and  $[\text{Fe}^{3+}]$  and  $[\text{Fe}^{2+}]$  are the concentrations of Fe<sup>3+</sup> and Fe<sup>2+</sup> (mol cm<sup>-3</sup>) in solution. The  $k_{\text{app}}$  of Fe<sup>2+/3+</sup> in anhydrous and water-containing ethaline at 298 K are listed in Table S4 and plotted in Figure 4c. The enhancement of  $k_{\text{app}}$  upon introduction of water to the DES mixture is clearly observed in Figure S14 as anticipated due to the direct relationship between  $k_{\text{app}}$  and  $k_{\text{f}}$  as given in eq. (4). With increasing temperature, the  $k_{\text{app}}$  generally also increases because higher temperatures increase the kinetic energy of molecules, which leads to more frequent and energetic collisions between reactant molecules. This increase in the frequency and energy of collisions increases the probability that reactant molecules will react, leading to a faster reaction rate. The observed increase in  $k_{\text{app}}$  of Fe<sup>2+/3+</sup>-ethaline with increasing temperature has also been reported by Kontturi and colleagues.[43]

The diffusion coefficients play a crucial role in electrochemical processes involving Fe<sup>2+</sup> and Fe<sup>3+</sup> ions. The rate of electron transfer reactions at an electrode surface is controlled by the diffusion of the reactant ions, which is influenced by their diffusion coefficients.[44] In Fe<sup>2+/3+</sup>-ethaline solutions, the diffusion coefficients were determined from limiting current measurements on a Pt RDE at various rotation speeds to examine the kinetics of the reaction and the effect of mass transport on the reaction rate. The ethaline was kept at constant Fe<sup>3+</sup> and Fe<sup>2+</sup> concentrations (50 mM), while the water content (0, 5, 10, 25 wt. %) and temperature (298 K – 323 K) were

varied. Using the Levich equation,[42] the diffusion coefficient was calculated from cathodic and anodic limiting currents using eq. (5a) and (5b), respectively.

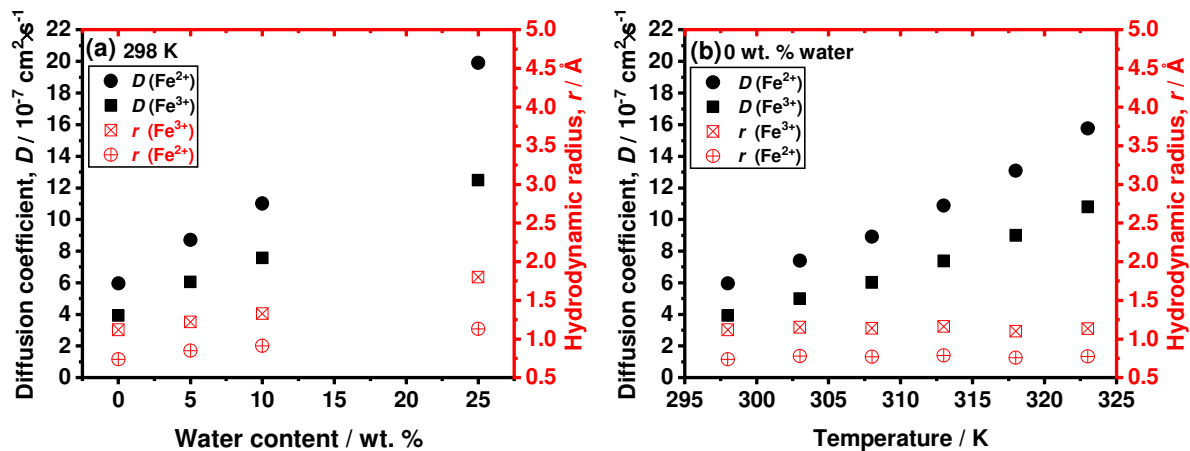
$$i_L = 0.627 n F D^{1/2} \rho \omega^{1/2} [Fe]_{bulk} \quad (5a)$$

$$i_L = 0.627 n F D^{1/2} \rho \omega^{1/2} [Fe]_{bulk} \quad (5b)$$

where  $i_L$  is the limiting current density,  $n$  is the number of transferred electrons,  $F$  is the Faraday constant,  $D$  is the diffusion coefficient,  $\rho$  is the viscosity,  $\rho$  is the density,  $[Fe]_{bulk}$  symbolizes the bulk concentration of  $Fe^{2+/3+}$ , and  $\omega$  is the rotation rate expressed as angular velocity.

The computed diffusion coefficients of  $Fe^{3+}$  and  $Fe^{2+}$  are plotted as a function of water content in Figure 5a and are listed in Table S5 at temperatures between 298 and 323 K. As the water content increases, both the  $Fe^{3+}$  and  $Fe^{2+}$  ions exhibit an increase in their diffusion coefficients. However,  $Fe^{2+}$  ions have a higher diffusion coefficient compared to  $Fe^{3+}$  ions at all water contents as seen in Figure S15. At water content  $\approx$  10 wt. %, the diffusion coefficients for the  $Fe^{2+}$  and  $Fe^{3+}$  ions in the investigated aqueous ethaline mixtures are still an order of magnitude smaller than their corresponding values in water ( $D_{Fe^{2+}} = 7.19 \times 10^{-6} \text{ cm}^2/\text{s}$  and  $D_{Fe^{3+}} = 6.04 \times 10^{-6} \text{ cm}^2/\text{s}$ ).[25,45]

When DES mixtures are heated, their viscosity decreases, which in turn increases the mobility of the ions and improves their diffusion coefficients. The enhancement in diffusion coefficients with increasing temperature has been supported previously. [43] As temperature increases, the solvent molecules become more disordered and less viscous, which lowers the resistance to the diffusion of ions, reducing the frictional force that impedes their movement and promoting their diffusion through the solvent. The experimental results presented in Figure S16 show that  $Fe^{2+}$  diffuses faster than  $Fe^{3+}$  in the temperature range of 298 to 303 K.



**Figure 5.** The (a) diffusion coefficients of  $\text{Fe}^{3+}$  and  $\text{Fe}^{2+}$  at 298 K, and (b) hydrodynamic radius of  $\text{Fe}^{2+}$  and  $\text{Fe}^{3+}$  ions in ethaline containing 0, 5, 10, or 25 wt. %  $\text{H}_2\text{O}$  at 298 – 323 K.

The hydrodynamic radii of  $\text{Fe}^{3+}$  and  $\text{Fe}^{2+}$  ions were determined using the Stokes-Einstein equation, which is based on the movement of spherical species in a continuum of solvent restricting the moving ions:[46]

$$D = \frac{k_B T}{6\pi\eta r} \quad (6)$$

Where  $r$  is the hydrodynamic radius,  $k_B$  is the Boltzmann constant,  $T$  is the temperature,  $\eta$  is the temperature-dependent viscosity, and  $D$  is the temperature-dependent diffusion coefficient.

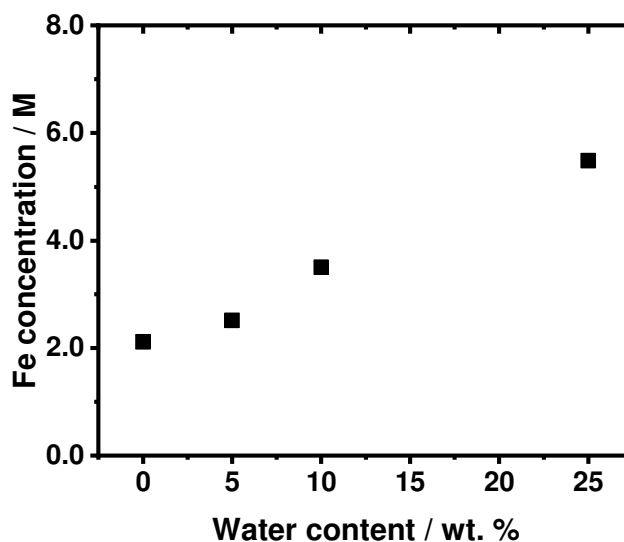
The hydrodynamic radii of  $\text{Fe}^{2+}$  and  $\text{Fe}^{3+}$  ions at 298 K are calculated to be 0.74  $\text{\AA}$  and 1.12  $\text{\AA}$ , respectively. The harder cation  $\text{Fe}^{3+}$  has the larger hydration shell which is commensurate with its lower diffusion coefficients at all water contents. The hydrodynamic radii of  $\text{Fe}^{3+}$  and  $\text{Fe}^{2+}$  ions decrease with increasing temperature as shown in Figure 5b.

### 3.4. Arrhenius fit and solubility

The temperature dependence of fluidity, conductivity, rate constant, and diffusivity were further investigated using Arrhenius model. The Arrhenius equation assumes linear relationship between  $\log x$  and inverse of temperature ( $T^{-1}$ ) as given in eq. (7). [47]

$$\log x = \log A - \frac{E_a}{RT} \quad (7)$$

where  $x$  refers to various properties such as fluidity ( $\eta^{-1}$ ), conductivity ( $\sigma$ ), rate constant ( $k$ ), diffusivity of  $\text{Fe}^{2+}$  ion ( $D_{\text{Fe}^{2+}}$ ) and diffusivity of  $\text{Fe}^{3+}$  ion ( $D_{\text{Fe}^{3+}}$ ).  $A$  is the pre-exponential factor,  $E_a$  is the activation energy,  $R$  is the gas constant, and  $T$  is the temperature. Figure S17 depicts the Arrhenius plots for fluidity, conductivity, rate constant, and diffusivity of  $\text{Fe}^{2+}$  or  $\text{Fe}^{3+}$  ion at temperature range of 298 – 323 K in 5 K increments. The Arrhenius fit parameters are recorded in Table S6. Figure S18 shows that for water content equal to or less than 10 wt. %, the activation energies for conductivity, rate constant, and diffusivity of  $\text{Fe}^{3+}$  ion decreases with increasing water content. The activation energy for diffusivity of  $\text{Fe}^{3+}$  ion exhibits a slightly greater dependence on temperature, followed by conductivity and rate constant. Alternatively, the addition of water does not affect the activation energy for  $\text{Fe}^{2+}$  diffusivity. At 0 wt. % water, the activation energies for fluidity, conductivity, rate constant, and diffusivity of  $\text{Fe}^{2+}$  or  $\text{Fe}^{3+}$  ion are similar, which proposes that the temperature impacts these properties in the same way.



**Figure 6.** Maximum solubility of  $\text{FeCl}_2/\text{FeCl}_3$  in ethaline as a function of water content.

Furthermore, the solubility of iron chloride salts in ethaline-water mixtures can be observed in Figure 6, which displays the results obtained through atomic absorption spectroscopy. The graph depicts an increase in the solubility of iron chloride salts as the water content in the ethaline solution increases. Because iron chloride salts exhibit high solubility (> 1 M) in DESs, it becomes feasible to utilize the Fe<sup>2+/3+</sup> redox couple in redox flow batteries.

#### 4. Conclusions

In this work, the electrochemical stability properties of ethaline, a greener electrolyte, were investigated through the redox couple Fe<sup>2+/3+</sup> as electrochemical probe in light of future use in redox flow batteries. The mass transport parameters ( $D_{Fe^{2+/3+}}$ ,  $\lambda_{Fe^{2+/3+}}$ ) as well as the kinetic parameters such as the charge transfer coefficients ( $\alpha_{Fe^{2+/3+}}$ ) exchange current density ( $i_0$ ) and reaction rate constant ( $k_{Fe^{2+/3+}}$ ) were determined as a function of gradual addition of water and increase in temperature. The results show that the introduction of defined amounts of water into the DES solvent system at 298 K – 323 K resulted in a decrease in viscosity and density of ethaline, and a three-fold increase in its ionic conductivity. The ~2% decrease in the electrochemical stability window is due to the decomposition of water that produces hydrogen gas. Owing to the lowered viscosity of ethaline, the  $D_{Fe^{2+/3+}}$ ,  $\lambda_{Fe^{2+/3+}}$  and  $\lambda_{Fe^{2+/3+}}$  increased after incorporation of water as minority solvent component into the DES. With an increased temperature, the kinetic energy and mobility of ions were enhanced resulting in an increased  $D_{Fe^{2+/3+}}$ ,  $\lambda_{Fe^{2+/3+}}$  and  $\lambda_{Fe^{2+/3+}}$ . The solubility of iron chloride salts in ethaline increases with increasing water content. The activation energy for conductivity, rate constant, and diffusivity of Fe<sup>3+</sup> ions decrease with water content up to 10 wt. %. However, beyond 10 wt. % water addition, a slight increase in activation energy can be seen. These findings provide an avenue to improve the physical and transport properties of other existing and future DESs by analytical hydration and increasing temperature, without significant reduction in electrochemical stability window, and could lead to the development of an economically viable electrolyte for redox flow batteries. The work presented herein suggests that higher-performance and lower-cost RFBs can be achieved in an environmentally compatible and sustainable manner by a “hydrated-DES” approach.



### **CRedit authorship contribution statement**

**Desiree Mae Prado:** Conceptualization, Methodology, Validation, Investigation, Formal analysis, Writing – Original Draft. **Xiaochen Shen:** Conceptualization, Methodology, Validation, Investigation, Formal analysis. **Robert Savinell:** Supervision, Conceptualization, Methodology, Writing - Review & Editing. **Clemens Burda:** Supervision, Conceptualization, Methodology, Writing - Review & Editing.

### **Declaration of competing interest**

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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